# Root cause analysis and succesful modifications to eliminate hot spots in SRU at MOL's Danube Refinery

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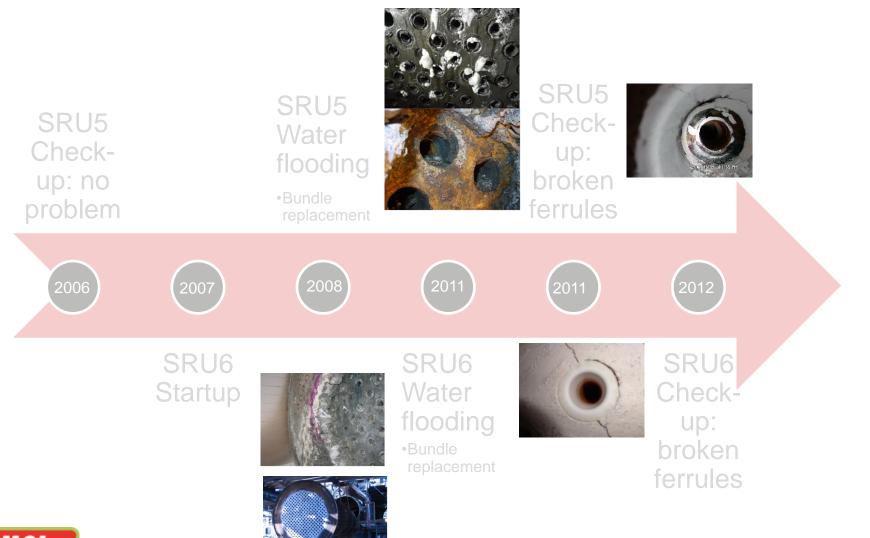
# SRU units

	SRU4	SRU5	SRU6
Startup	1992	2000	2007
Capacity	85 t/d	90 t/d	90 t/d
Feed	AAG: amine acid gas SWS: Sour water stripper gas	AAG: amine acid gas SWS: Sour water stripper gas	AAG: amine acid gas SWS: Sour water stripper gas
Steam pressure	18 (14) barg	52 (45) barg	52 (45) barg
Steam temperature	~180°C	263°C	263°C

SRU1,2,4,7 units had shown no problems with bundle walls SRU3,5,6 units developed serious problems within short operation times



## Timeline





## Damage details: SRU5 unit



Large percentage of ceramic ferrules were broken or cracked





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Outlet bundle wall intact



Refractory wall support pins corroded away



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Bundle wall and tube weldings corroded

Tube endings funnelled in, thinned around the ending

#### More than 57 leaking welding





## Repairs of SRU5 unit (2008)

Bundle lining was replaced according original design

Inlet side bundle wall was replaced

Ceramic ferrules and refractory wall were replaced according original design

Refractory wall support pins were modified



## Damage details: SRU6 unit (2011)

Refractory wall separated from bundle wall



Large percentage of ceramic ferrules were broken or cracked



Refractory wall support pins burned away



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#### Outlet bundle wall was intact

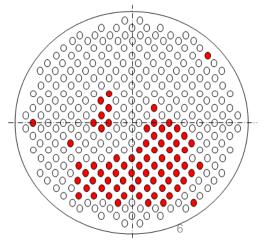
Bundle wall and line endings were corroded

Tube inlets were funnelled, thinned around the weldings

More than 75 inlets leaked at low pressure testing, replacement needed







# Damage investigation

## Possible damage mechanism:

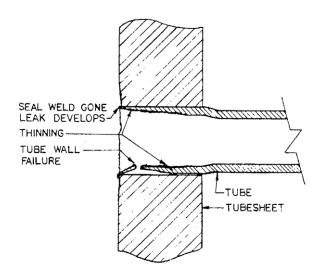
- High temperature S-corrosion damages overheated areas like bundle wall and tube inlets and weldings (high prob.)
- Acid dew corrosion during S/U and S/D. (low prob.)

## **Possible counteractions**

- Cr alloy materials instead of carbon steel
- Reducing surface temperature
  - Lower bundle wall thickness
  - Reduced welding distance from feed water
  - Prevent ferrule and refractory wall cracks, protecting the less cooled areas from



TYPICAL TUBE END DETERIORATION AND FAILURES



## Repairs and modifications: SRU6 unit (2011)

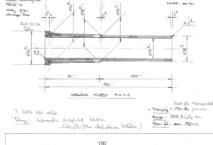
Bundle lining replaced according original design

# Tube ending welds were modified for better cooling

Ceramic ferrules were changed to more robust type, refractory wall remained original design

2012: Ferrules were coated with thick heat-resistant fibre insulation to avoid stress fractures due to wall movements







## Internal benchmark: Ferrule+Refractory types



#### Similarities:

- Fix bundle
- Concrete refractory + ceramic ferrules over the bundle wall
- Boiler material quality
- Processing capacity (90 t/d)



#### Differences

• Inlet side bundle wall thickness



#### Modifications:

- Additional 5 mm fibre insulation between bundle and refractory walls
- Stronger ferrules and wall support pins, weldings



#### Results

- Cracked ferrules within a few years of operation
- · Beginning or leaking corrosion and funneling



## Internal Benchmark: Block ferrules and Other protections



#### Similarities:

- Fix bundle
- Boiler material quality
- 30 mm bundle walls



#### Differences

- Tube size and number
- Waterside pressure
- Heat distributor wall



#### **Modifications**

• Replacements of ferrules to block type in 2 units



#### Results

• No breaking or corrosion







# Summary

## Damage mechanism:

• High temperature S-corrosion at hot parts of the inlet side tube endings

# Suggestions:

- Thin bundle wall
- Corner of half V welds at tube endings
- Block type ferrules instead of tubular ferrule+refractory wall
- Fibre insulation coated ferrules
- Heat distributor wall (optional)





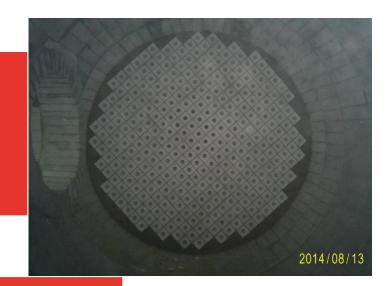




## Results



# 2 SRU unit modified during 2014-2015





#### Modifications:

- Bundle wall replaced (35 mm)
- Bundle lines replaced
- Tube weldings: corner welds
- Refractory+ferrules replaced by block type ferrules
- Heat distributor wall deemed unnecessary.

#### Testing:

• 2017 check-up found 2 cracked ferrule after extreme testing

